## Mechanics of Solids (MEC2112/AEC2112) 2024-25

## Tutorial 3 (Unit-2)

1. In a state of plane strain, the strain components associated with the x-y axes are

$$\epsilon_{xx} = 800 \times 10^{-6}$$
 $\epsilon_{yy} = 100 \times 10^{-6}$ 
 $\gamma_{xy} = -800 \times 10^{-6}$ 

Find the strain components in a new coordinate system (x' - y') such that x' is at an angle of  $45^{\circ}$  with x.

2. The tensorial strain in a body is

$$[\epsilon] = \begin{bmatrix} 2 & -2 & 1 \\ -2 & 1 & 1 \\ 1 & 1 & 1 \end{bmatrix} \times 10^{-2}$$

in a coordinate system (x-y-z). Find the strain tensor in a new coordinate system (x'-y'-z') such that x' is along  $\hat{i}+\hat{j}$  and y' is in the direction of  $-\hat{i}+\hat{j}$ .

3. The state of stress in a body is

$$[\sigma] = \begin{bmatrix} 2 & 10 & 5 \\ 10 & 2 & 1 \\ 5 & 1 & 2 \end{bmatrix} MPa.$$

Find the strain components if Young's modulus is 1 GPa and Poison's ratio is 0.25.

4. The displacement field for a body is described by

$$u(x, y, z) = 0.05x + 0.01y$$
  
 $v(x, y, z) = 0.01x + 0.02y.$   
 $w(x, y, z) = 0.01z.$ 

Find the stress tensor, if Young's modulus is 1 GPa and Poison's ratio is 0.25. [Hint: Use the relation between E,  $\nu$  and  $\lambda$ ,  $\mu$ ].

- 5. A cube of side 1 cm is confined by rigid walls on all sides and is heated by 30°C. What would be the stress (i.e., stress components) developed in the cube? Take  $\alpha$  as 0.001 /°C
- 6. If Young's modulus is 1 GPa and Poison's ratio is 0.25, obtain the stiffness matrix and compliance matrix for plane stress as well as plane strain cases. [Hint: The relation between E,  $\nu$  and  $\lambda$ ,  $\mu$  may be useful].

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1) Let the transformed Strain components are: 
$$Ex'x'$$
,  $Ey'y'$ ,  $Yx'y'$ 

$$Ex'x' = \frac{Exx + Eyy}{2} + \frac{Exx - Eyy}{2} \cos 2\theta + \frac{Yxy}{2} \sin 2\theta$$

$$Ey'y' = \frac{Exx + Eyy}{2} - \frac{Exx - Eyy}{2} \cos 2\theta - \frac{Yxy}{2} \sin 2\theta$$

$$Yx'y' = -(Exx - Eyy) \sin 2\theta + Yxy \cos 2\theta$$

$$Exx = 800 \times 10^{-6}$$

$$Ey'y' = \frac{800 \times 10^{-6}}{2} + \frac{800 \times 10^{-6} + 100 \times 10^{-6}}{2} + \frac{800 \times 10^{-6} - 100 \times 10^{-6}}{2} + \frac{800 \times 10^{-6} - 100 \times 10^{-6}}{2} + \frac{900 \times 10^{-6} - 400 \times 10^{-6}}{2} + \frac{900 \times 10^{$$

$$Y_{x}'y' = -(800 \times 10^{-6} - 100 \times 10^{-6}) \times 1 + (-800 \times 10^{-6}) \times 0$$

$$Y_{x}'y' = (-700 \times 10^{-6}) + 0 = -700 \times 10^{-6}$$

$$[E] = \begin{bmatrix} 2 & -2 & 1 \\ -2 & 1 & 1 \\ 1 & 1 & 1 \end{bmatrix} \times 10^{-2}$$

The new axes are:

z' is along 
$$\hat{i}+\hat{j}$$

y' is along  $-\hat{i}+\hat{j}$ 

The dir of x' is 1 (1,1,0)

Z' axis will remain unchanged and orthogonal to both x' and y'  $\Rightarrow$  so it remains in dir (0,0,1)

## Rotation Matrix

Tensor
$$[E'] = [R]^{T} [E] [R]$$

$$[E] = \begin{bmatrix} 2 & -2 & 1 \\ -2 & 1 & 1 \\ 1 & 1 & 1 \end{bmatrix} \times 10^{-2}$$

$$[R]^{T} [E] = \begin{bmatrix} \frac{1}{52}(2) + \frac{1}{52}(2) & \frac{1}{52}(2) + \frac{1}{52}(1) & \frac{1}{52}(1) + \frac{1}{52}(1) \\ -\frac{1}{52}(2) + \frac{1}{52}(2) & \frac{1}{52}(2) + \frac{1}{52}(1) & \frac{1}{52}(1) + \frac{1}{52}(1) \\ 1 & 1 & 1 \end{bmatrix}$$

$$[R]^{T} [E] = \begin{bmatrix} \frac{1}{52}(2) + \frac{1}{52}(2) & \frac{1}{52}(2) + \frac{1}{52}(1) & \frac{1}{52}(1) + \frac{1}{52}(1) \\ \frac{1}{52}(1) + \frac{1}{52}(1) & \frac{1}{52}(1) + \frac{1}{52}(1) \\ 1 & 1 & 1 \end{bmatrix}$$

$$[R]^{T} [E] = \begin{bmatrix} 0 & -\frac{1}{52}(2) + \frac{1}{52}(2) & \frac{1}{52}(2) + \frac{1}{52}(1) & \frac{1}{52}(1) + \frac{1}{52}(1) \\ \frac{1}{52}(1) + \frac{1}{52}(1) & \frac{1}{52}(1) \\ \frac{1}{52}(1) + \frac{1}{52}(1) \\ \frac{1}{52}(1) + \frac{1}{52}(1) & \frac{1}{52}(1) + \frac{1}{52}(1) \\ \frac{1}{52}(1) + \frac{1}{52}(1) + \frac{1}{52}(1) \\ \frac{1}{52}(1) + \frac{1}{52}(1) + \frac{1}{52}(1) + \frac{1}{52}(1) \\ \frac{1}{52}(1) + \frac{1}{52}(1) + \frac{1}{52}(1) \\ \frac{1}{52}(1) + \frac{1}{52}(1) + \frac{1}{52}(1) \\ \frac{1}{52}(1) + \frac{1}{52}(1) + \frac{1}{52}(1) + \frac{1}{52}(1) \\ \frac{1}{52}(1) + \frac{1}{52}(1) + \frac{1}{52}(1) + \frac{1}{52}(1) + \frac{1}{52}(1) + \frac{1}{52}(1) \\ \frac{1}{52}(1) + \frac{1}{52}(1) +$$

$$\begin{bmatrix} E' \end{bmatrix} = \begin{bmatrix} 0 \cdot \frac{1}{\sqrt{2}} + \begin{pmatrix} -\frac{1}{\sqrt{2}} \end{pmatrix} \cdot \frac{1}{\sqrt{2}} + \langle 2 \cdot 0 & 0 \cdot -\frac{1}{\sqrt{2}} + \begin{pmatrix} -\frac{1}{\sqrt{2}} \end{pmatrix} \cdot \frac{1}{\sqrt{2}} + \langle 2 \cdot 0 & 0 \cdot -\frac{1}{\sqrt{2}} + \langle -\frac{1}{\sqrt{2}} \end{pmatrix} \cdot \frac{1}{\sqrt{2}} + \langle 2 \cdot 0 & 0 \cdot 0 + \langle 2 \cdot 1 \rangle \\ - \sqrt{2} \cdot \frac{1}{\sqrt{2}} + \frac{1}{\sqrt{2}} \cdot \frac{1}{\sqrt{2}} + 0 \cdot 0 & -\sqrt{2} \cdot \frac{1}{\sqrt{2}} + \frac{1}{\sqrt{2}} \cdot \frac{1}{\sqrt{2}} + 0 \cdot 0 & -\sqrt{2} \cdot 0 + \frac{1}{\sqrt{2}} \cdot 0 + 0 \cdot 1 \\ 1 \cdot \frac{1}{\sqrt{2}} + \frac{1}{\sqrt{2}} \cdot \frac{1}{\sqrt{2}} + 1 \cdot 0 & 1 \cdot 0 + 1 \cdot 1 \end{bmatrix}$$

$$\begin{bmatrix} E' \end{bmatrix} = \begin{bmatrix} -1 & -1 & 52 \\ 2 & 2 & 0 \\ -1 & \frac{1}{2} & 0 \end{bmatrix} \times 10^{-2} \quad \begin{bmatrix} E' \end{bmatrix} = \begin{bmatrix} -0.5 \times 10^{-2} & -0.5 \times 10^{-2} & 1.41 \times 10^{-2} \\ -1.0 \times 10^{-2} & 0.5 \times 10^{-2} & 0 \\ 1.41 \times 10^{-2} & 0 & 1.0 \times 10^{-2} \end{bmatrix}$$

Given: 
$$[T] = \begin{bmatrix} 2 & 10 & 5 \\ 10 & 2 & 1 \\ 5 & 1 & 2 \end{bmatrix} MPa$$

$$f = 1 GPa$$
;  $\vartheta = 0.25$   
 $+ \Upsilon(\tau) = 2 + 2 + 2 = 6 M Pa$ 

$$[E] = \begin{bmatrix} 0.0005 & 0.001 & 0.0005 \\ 0.01 & 0.0005 & 0.001 \\ 0.005 & 0.001 & 0.0005 \end{bmatrix}$$

$$4 \qquad \mathcal{L}(x,y,z) = 0.05 \times + 0.01 y$$

$$\mathcal{L}(x,y,z) = 0.01 \times + 0.02 y$$

$$\omega(x, y, z) = 0.01z$$

$$\begin{aligned}
&\mathcal{E}_{xx} = \frac{\partial u}{\partial x} & \mathcal{E}_{xy} = \frac{1}{2} \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) \\
&\mathcal{E}_{yy} = \frac{\partial v}{\partial y} & \mathcal{E}_{xz} = \frac{1}{2} \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \\
&\mathcal{E}_{zz} = \frac{\partial w}{\partial z} & \mathcal{E}_{yz} = \frac{1}{2} \left( \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right)
\end{aligned}$$

$$= \frac{\partial y}{\partial z} = \frac{1}{2} \left( \frac{\partial y}{\partial z} + \frac{\partial w}{\partial y} \right)$$

$$[E] = \begin{bmatrix} 0.05 & 0.01 & 0 \\ 0.01 & 0.02 & 0 \\ 0 & 0 & 0.01 \end{bmatrix}$$

$$\begin{aligned}
f(xy) &= \frac{1}{2} \left( \frac{\partial y}{\partial y} + \frac{\partial v}{\partial z} \right) = \frac{1}{2} \left( \frac{\partial (0+0)}{\partial (0+0)} \right) \\
&= 0.01 \\
f(xz) &= \frac{1}{2} \left( \frac{\partial y}{\partial z} + \frac{\partial (0+0)}{\partial z} \right) = \frac{1}{2} \left( \frac{\partial (0+0)}{\partial z} \right) = 0 \\
f(yz) &= \frac{1}{2} \left( \frac{\partial v}{\partial z} + \frac{\partial (0+0)}{\partial z} \right) = \frac{1}{2} \left( \frac{\partial (0+0)}{\partial z} \right) = 0
\end{aligned}$$

$$[T] = \lambda + (\epsilon)[T] + 2\mu[\epsilon]$$

$$\lambda = \underbrace{E\nu}_{(1-2\nu)}$$

$$\begin{cases}
E = \begin{bmatrix} 0.05 & 0.01 & 0 \\
0.01 & 0.02 & 0 \\
0 & 0 & 0.01
\end{cases}$$

$$\begin{cases}
A = \underbrace{EV}_{(1+V)}(1-2V) \\
U = \underbrace{I000}_{2.5} = \underbrace{1000}_{2.5} \\
1 = \underbrace{1000}_{2.5} = \underbrace{1000}_{2.5}$$

$$= \underbrace{1000}_{2.5} = \underbrace{1000}_{2.5}$$

$$A = \frac{1000 \times 0.25}{(1+0.25)(1-2\times0.25)} = \frac{250}{1.25\times0.5} = \frac{250}{6.625} = 400 \text{ MPa}$$

$$[T] = 400 \times 0.09 [T] + 2 \times 400 \times \begin{bmatrix} 0.05 & 0.01 & 0 \\ 0.01 & 0.02 & 0 \\ 0 & 0 & 0.01 \end{bmatrix}$$

$$= \begin{bmatrix} 32 & 0 & 0 \\ 0 & 32 & 0 \\ 0 & 0 & 32 \end{bmatrix} + \begin{bmatrix} 40 & 8 & 0 \\ 8 & 16 & 0 \\ 0 & 0 & 8 \end{bmatrix}$$

$$\begin{bmatrix}
 \end{bmatrix} = \begin{bmatrix}
 72 & 8 & 0 \\
 8 & 48 & 0 \\
 0 & 0 & 40
 \end{bmatrix}
 MPa$$

$$\begin{array}{rcl}
\text{E-Thermal} & - & \times & 1 \\
& = & 0.001 \times 30 \\
& = & 0.03
\end{array}$$

$$6$$

$$A = \underbrace{FV}_{(1+V)(1-2V)}$$

$$\mu = \underline{E} = \underline{1000} = 400 \,\text{M/z}$$
 $2(1+0) = 2(1+0.25)$ 

$$A = \frac{1000 \times 0.25}{(1+0.25)(1-2\times0.25)} = \frac{250}{1.25 \times 0.5} = \frac{250}{0.625}$$

$$= 400 \text{ MPa}$$

$$\begin{bmatrix} \nabla x \\ \nabla y \end{bmatrix} = \begin{bmatrix} \underline{E} & \underline{V}\underline{E} & 0 \\ \underline{I-V^2} & \underline{I-V^2} & 0 \\ \underline{V}\underline{E} & \underline{E} & 0 \\ \underline{I-V^2} & \underline{I-V^2} & 0 \\ 0 & 0 & \underline{H} \end{bmatrix} \begin{bmatrix} \underline{E} \\ \underline{Y} \\ \underline{$$

$$\begin{bmatrix} \zeta \end{bmatrix} = \begin{bmatrix} \frac{E}{1-\sqrt{2}} & \frac{\sqrt{2}E}{1-\sqrt{2}} & 0 \\ \frac{\sqrt{2}E}{1-\sqrt{2}} & \frac{E}{1-\sqrt{2}} & 0 \\ 0 & 0 & 2 \end{bmatrix}$$

$$\frac{E}{1-v^2} = \frac{1000}{1-(0.25)^2} = \frac{1000}{0.9375} = 1066.67$$
MPa

$$\frac{\sqrt{E}}{1-v^2} = \frac{0.25 \times 1000}{0.9375} = \frac{250}{0.9375} = \frac{266.67}{MPa}$$

$$\frac{H}{2} = \frac{400}{2} = 200 \text{ MPa}$$

$$\begin{bmatrix} C \end{bmatrix} = \begin{bmatrix} 1066.67 & 266.67 & 0 \\ 266.67 & 1066.67 & 0 \\ 0 & 0 & 200 \end{bmatrix} HPa$$

## Plain Strain Case:

$$\begin{bmatrix} \nabla_{\chi} \\ \nabla_{y} \\ \nabla_{x} \end{bmatrix} = \begin{bmatrix} \frac{E}{(1+\nu)(1-2\nu)} & \frac{\nu E}{(1+\nu)(1-2\nu)} & 0 \\ \frac{\nu E}{(1+\nu)(1-2\nu)} & \frac{E}{(1+\nu)(1-2\nu)} & 0 \\ 0 & 0 & \frac{H}{2} \end{bmatrix} \begin{bmatrix} \varepsilon_{\chi} \\ \varepsilon_{y} \\ \gamma_{\chi y} \end{bmatrix}$$

$$\begin{bmatrix} C \end{bmatrix} = \begin{bmatrix} \frac{E}{(1+\nu)(1-2\nu)} & \frac{\nu E}{(1+\nu)(1-2\nu)} & 0 \\ \frac{\nu E}{(1+\nu)(1-2\nu)} & \frac{E}{(1+\nu)(1-2\nu)} & 0 \\ 0 & 0 & \frac{H}{2} \end{bmatrix}$$

$$\frac{E}{(1+v)(1-2v)} = \frac{1000}{(1+0.25)(1-2\times0.25)} = \frac{1000}{1.25\times0.5} = \frac{1000}{0.625}$$

$$= 1600 \text{ MPa}$$

$$\frac{E}{(1+v)(1-2v)} = \frac{0.25\times1000}{0.625} = \frac{250}{0.625} = 400 \text{ MPa}$$

$$\begin{bmatrix} C \end{bmatrix} = \begin{bmatrix} 1600 & 400 & 0 \\ 400 & 1600 & 0 \\ 0 & 0 & 200 \end{bmatrix}$$

$$\begin{bmatrix} S \end{bmatrix} = \begin{bmatrix} \frac{1-v^2}{E} & -\frac{v}{E} & 0 \\ -\frac{v}{E} & \frac{1-v^2}{E} & 0 \\ 0 & 0 & \frac{1}{\mu} \end{bmatrix}$$

$$\frac{M}{2} = 200 \text{ MPa} \qquad \frac{1 - v^2}{E} = \frac{1 - (0.25)^2}{(000)} = \frac{0.9375}{(000)} = 0.0009375$$

$$\begin{bmatrix} C \end{bmatrix} = \begin{bmatrix} 1600 & 400 & 0 \\ 400 & 1600 & 0 \\ 0 & 0 & 200 \end{bmatrix} \qquad \frac{-0}{E} = -\frac{0.25}{1000} = -0.00025$$

$$\begin{bmatrix} C \end{bmatrix} = \begin{bmatrix} 1 - v^2 - v \\ E \end{bmatrix} = \begin{bmatrix} 1 - v^2 - v \\ E \end{bmatrix} = \begin{bmatrix} 1 - v^2 - v \\ 0 \end{bmatrix} \qquad \begin{bmatrix} C \end{bmatrix} = \begin{bmatrix} 1 - v^2 - v \\ 0 \end{bmatrix} = \begin{bmatrix} 1 - v^2 - v \\ 0 \end{bmatrix} \qquad \begin{bmatrix} C \end{bmatrix} = \begin{bmatrix} 0.0009375 - 0.00025 \\ 0.00025 \end{bmatrix} = \begin{bmatrix} 0.0009375 - 0.00025 \\ 0.00025 \end{bmatrix}$$

MPa-1

$$\frac{1}{E} = \frac{1000}{1000} = 0.001$$

$$\frac{-\sqrt{2}}{E} = \frac{-0.25}{1000} = -0.00025$$

$$[S] = \begin{bmatrix} 0.001 & -0.00025 & 0 \\ -0.00025 & 0.001 & 0 \\ 0 & 0.0025 \end{bmatrix} MPa^{-1}$$

Stiffness matrix for plane strain
$$\begin{bmatrix} C \end{bmatrix} = \begin{bmatrix} 1600 & 400 & 0 \\ 400 & 1600 & 0 \\ 0 & 0 & 200 \end{bmatrix} MPa$$

Compliance matrix for plane stress:

$$[S] = \begin{bmatrix} 0.0009375 & -0.00025 & 0 \\ -0.00025 & 0.0009375 & 0 \\ 0 & D & 0.0025 \end{bmatrix}$$

$$MPa^{-1}$$

Compliance matrix for plane strain:
$$[S] = \begin{bmatrix} 0.001 & -0.00025 & 0 \\ -0.00025 & 0.001 & 0 \\ 0 & 0.0025 \end{bmatrix}$$
MPa